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# Summary of Description \& Claims 

eXp7™ - an eXponential Shoe Sizing System - A shoe sizing system that increments sizes by a percentage increase instead of a fixed increment, e.g. $1 / 6^{\prime \prime} \& 1 / 3 \mathrm{~cm}$ for $1 / 2$ size increments in the Barleycorn \& Paris Point systems and, $1 / 2 \mathrm{~cm}$ \& $3 / 4 \mathrm{~cm}$ for the 5 mm \& $71 / 2 \mathrm{~mm}$ increments in the MondoPoint system. The increment is 7 steps per inch around a $\sim 94 / 5^{\prime \prime}, 24.85 \mathrm{~cm}$ foot ( $9.3^{\prime \prime}$ to $10.3^{\prime \prime}, 23.61$ to 26.15 cm ) a non-linear progression that increases the increment value as size increases. Using $5.88 \%$ toe room the increment size at $341 / 4$ IT|EU is $1 / 3 \mathrm{~cm}$ ( $1 / 2$ size Paris Point), and at 9.3 UK it is $1 / 6^{\prime \prime}(1 / 2$ size Barleycorn).
Better Fittings \& Manufacturing Efficiency - Since this is a ratio based system it produces a more consistent and usable coverage of the sizes providing better fittings which may also reduce the number of sizes needed to cover the the same size range.
Consistent Widths Across The Size Range Produces Easy Last Scaling - The spacing between the Widths is also a percentage increase offering the same benefits. Similar to the Brannock width system the width spacing is 3 increments of the width increment per $1 / 2$ size increment. This offers an additional division of the widths by 3 ( $1 / 3$ steps) by going up or down $1 / 2$ size and/or up or down in width. A $\pm 1 / 2$ size adjustment within the same width will adjust the width by $\pm 1 / 3$ step and a $\pm 1$ width adjustment with a $\mp 1 / 2$ size adjustment will adjust the width by $\pm^{2} / 3$ step. In the Brannock system a $1 / 2$ size increase of foot length is $1 / 6^{\prime \prime}$ while the width increases by $1 / 16^{\prime \prime}$. This Width:Length ratio of $371 / 2 \%=100 \times 6 \div 16(3 / 8)$ produces a consistent ratio for the D width across the whole size range but for all other widths this produces width spreading for the smallest sizes, an $183 / 4 \%$ differential, while for the largest sizes width squeezing, a $12^{1 / 6} \%$ differential, a $>6 \%$ difference, graph on pg7. The width curves become more curved for the widths further away from the D width. This means that the width increase step becomes larger in size for the smaller sizes relatively speaking, and vice-versa, smaller width increase step for the larger sizes. By using percentage scaling this problem is eliminated. Instead of using the fixed increment values for length and width of $1 / 6^{\prime \prime} \& 1 / 16^{\prime \prime}$ respectively the relationship between length \& width is: Width Spacing Factor $=\left(\right.$ Foot Increment Factor) ${ }^{3}$ providing a consistent percentage for all widths across the size range. Width:Length ratio percentages associated with labels are: AAA A $301 / 8$, AA B $31 \frac{1}{2}$, A C $327 / 8$, B D $343 / 8$, C E $357 / 8$, D F $371 / 2$, E G $391 / 5$, EE H $407 / 8$, EEE I $42^{3} / 4$. This is not as spread out so alignment with conventional width values will not line up and this can be extended to 4A and 5E or more.
$5.88 \% 27 \div 25^{1 / 2}$ Toe Room, $1 \frac{1}{2} \mathrm{~cm}$, using a $25^{1} / 2 \mathrm{~cm}$ Foot and a 27 cm Last, is used as the Origin and minimum average amount for Barleycorn \& Paris Point sizing but more could be used. In width adjustment through a $\pm 1 / 2$ size adjustment this corresponds to $71 / 2 \%$ \& $43 / 8 \%$. If $62 / 3 \%$ is used then toe room through width adjustment would be $81 / 4 \% \& 51 / 8 \%$ and the Barleycorn \& Paris Point Last size specification would be greater. The Toe Room specification does not limit toe box lengthening for styling purposes rather this is the minimum toe room requirement.

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BY: $\operatorname{eXp} 7^{\text {™ }}$ Size Scaling by JSG ${ }^{\text {M }}$ (Attribution) NC: Non-Commercial ND: No Derivative Works.

# Foot Length and Equivalent Paris Point \& Barleycorn Sizing using 5.88\% Toe Room 

## A MondoPoint eXponential Scaling Overlay

Weight Bearing Measurement



Reference values specified in mm (MondoPoint)
Foot Increment Factor $={ }^{\mathbf{1 0}} \sqrt{40^{1 / 2} \div 35}=1.01470242408$
(M) or $\mathbf{X}$ (W) as decimal.

TR $=27 \div 25^{½}=1.05882352941 ; 1 ½ \mathrm{~cm}$ TR @ $25^{½}$ cm Foot
Foot. $\mathrm{mm}=10 \times$ Last. $\mathbf{c m} \div$ TR ; Foot.in $=$ Foot. $m m \div 25^{2 / 5}$; Last.in $=T R \times$ Foot.in
IT|EU = $1 ½ \times$ Last.cm ; [Mx|UK|usM|usW] = IT|EU $\div 1.27-[2512|25| 24 \mid 22 ½]$

## Widths

Width.mm A Weight Bearing Measurement

|  | -Percent of Foot.mm Length |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | \| $-W i d t h$ |  | $\rightarrow$ (Roma | Numerals | are the Pr | erred Wid | Labeling) |  | $\underset{\text { EEE }}{\mathbf{X}}$ |
|  | $\longrightarrow$ II | III | IV | V | VI | VII | VIII | IX |  |
| exp7 | $\longrightarrow$ AAA | AA | A | B | C | D | E | EE |  |
| Size | $\longrightarrow 30.13$ | 31.48 | 32.88 | 34.36 | 35.89 | 37.50 | 39.18 | 40.93 | 42.76 |
|  | A3 | A2 | A | B | C | D | E | E2 | E3 |
| 6x5 | 61.7 | 64.5 | 67.4 | 70.4 | 73.5 | 76.8 | 80.3 | 83.9 | 87.6 |
| 6x6 | 62.6 | 65.4 | 68.4 | 71.4 | 74.6 | 78.0 | 81.4 | 85.1 | 88.9 |
| 6x7 | 63.5 | 66.4 | 69.4 | 72.5 | 75.7 | 79.1 | 82.6 | 86.3 | 90.2 |
| 6x8 | 64.5 | 67.4 | 70.4 | 73.5 | 76.8 | 80.3 | 83.9 | 87.6 | 91.5 |
| $6 \mathbf{} 9$ | 65.4 | 68.4 | 71.4 | 74.6 | 78.0 | 81.4 | 85.1 | 88.9 | 92.9 |
| $7 \times 0$ | 66.4 | 69.4 | 72.5 | 75.7 | 79.1 | 82.6 | 86.3 | 90.2 | 94.2 |
| 7×1 | 67.4 | 70.4 | 73.5 | 76.8 | 80.3 | 83.9 | 87.6 | 91.5 | 95.6 |
| 7×2 | 68.4 | 71.4 | 74.6 | 78.0 | 81.4 | 85.1 | 88.9 | 92.9 | 97.0 |
| $7 \times 3$ | 69.4 | 72.5 | 75.7 | 79.1 | 82.6 | 86.3 | 90.2 | 94.2 | 98.5 |
| $7 \times 4$ | 70.4 | 73.5 | 76.8 | 80.3 | 83.9 | 87.6 | 91.5 | 95.6 | 99.9 |
| 7×5 | 71.4 | 74.6 | 78.0 | 81.4 | 85.1 | 88.9 | 92.9 | 97.0 | 101.4 |
| $7 \times 6$ | 72.5 | 75.7 | 79.1 | 82.6 | 86.3 | 90.2 | 94.2 | 98.5 | 102.9 |
| $7 \times 7$ | 73.5 | 76.8 | 80.3 | 83.9 | 87.6 | 91.5 | 95.6 | 99.9 | 104.4 |
| 7×8 | 74.6 | 78.0 | 81.4 | 85.1 | 88.9 | 92.9 | 97.0 | 101.4 | 105.9 |
| $7 \times 9$ | 75.7 | 79.1 | 82.6 | 86.3 | 90.2 | 94.2 | 98.5 | 102.9 | 107.5 |
| $8 \mathbf{0}$ | 76.8 | 80.3 | 83.9 | 87.6 | 91.5 | 95.6 | 99.9 | 104.4 | 109.0 |
| $8 \mathbf{1}$ | 78.0 | 81.4 | 85.1 | 88.9 | 92.9 | 97.0 | 101.4 | 105.9 | 110.7 |
| $8 \mathbf{8}$ | 79.1 | 82.6 | 86.3 | 90.2 | 94.2 | 98.5 | 102.9 | 107.5 | 112.3 |
| $8 \mathbf{3}$ | 80.3 | 83.9 | 87.6 | 91.5 | 95.6 | 99.9 | 104.4 | 109.0 | 113.9 |
| $8 \mathbf{4}$ | 81.4 | 85.1 | 88.9 | 92.9 | 97.0 | 101.4 | 105.9 | 110.7 | 115.6 |
| $8 \mathbf{5}$ | 82.6 | 86.3 | 90.2 | 94.2 | 98.5 | 102.9 | 107.5 | 112.3 | 117.3 |
| $8 \mathbf{8}$ | 83.9 | 87.6 | 91.5 | 95.6 | 99.9 | 104.4 | 109.0 | 113.9 | 119.0 |
| $8 \mathbf{7}$ | 85.1 | 88.9 | 92.9 | 97.0 | 101.4 | 105.9 | 110.7 | 115.6 | 120.8 |
| 8× 8 | 86.3 | 90.2 | 94.2 | 98.5 | 102.9 | 107.5 | 112.3 | 117.3 | 122.6 |
| $8 \mathbf{7} 9$ | 87.6 | 91.5 | 95.6 | 99.9 | 104.4 | 109.0 | 113.9 | 119.0 | 124.4 |
| $9 \mathbf{0}$ | 88.9 | 92.9 | 97.0 | 101.4 | 105.9 | 110.7 | 115.6 | 120.8 | 126.2 |
| $9 \mathbf{1}$ | 90.2 | 94.2 | 98.5 | 102.9 | 107.5 | 112.3 | 117.3 | 122.6 | 128.0 |
| $9 \mathbf{2}$ | 91.5 | 95.6 | 99.9 | 104.4 | 109.0 | 113.9 | 119.0 | 124.4 | 129.9 |
| $9 \mathbf{3}$ | 92.9 | 97.0 | 101.4 | 105.9 | 110.7 | 115.6 | 120.8 | 126.2 | 131.8 |
| $9 \mathbf{4}$ | 94.2 | 98.5 | 102.9 | 107.5 | 112.3 | 117.3 | 122.6 | 128.0 | 133.8 |
| $9 \mathbf{5}$ | 95.6 | 99.9 | 104.4 | 109.0 | 113.9 | 119.0 | 124.4 | 129.9 | 135.7 |

## All values are in mm (MondoPoint)

The original Brannock Device® defines the D Width at $37 \frac{1}{2} \%$ of the Foot length and is consistent across the whole size range. For the other widths the Width:Length ratio varies across the sizes and the variance is greater for the widths further away from the D Width. Here the D Width, at $37 \frac{1}{2} \%$, is the origin and all other widths are scaled from it using the Width Spacing Factor which is defined as (Foot Increment Factor) ${ }^{3} \sim 1.04476$ thus making all widths a consistent percentage across the whole size range. The Ball of Foot Metatarsal Girth is set to $22 / 5 \times$ Width in the table, a nominal value that was obtained from some foot measurements. It could vary by $\pm 12 / 5 \%(2.3 \overline{6}-2.4 \overline{3})$ or more. This base $22 / 5$ Girth:Width ratio is in the ball park but could probably use some more fine tuning and can also be adjusted to desired needs e.g. larger for thicker socks. This applies to a lesser extent to the Width table.

# Girths 

## Girth. $\mathrm{mm} \approx \mathbf{2}^{2 / 5} \times$ Width.mm

Table Values are Non-Weight Bearing, (Weight Bearing Adjustment Scalar)

|  | -Percent of Foot.mm Length |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\longrightarrow$ II | III | IV | V | VI | VII | VIII | IX | X |
| eXp7 | $\longrightarrow$ AAA | AA | A | B | C | D | E | EE | EEE |
| Size | $\longrightarrow 72.30$ | 75.54 | 78.92 | 82.45 | 86.14 | 90.00 | 94.03 | 98.24 | 102.6 |
|  | (743) | (78) | (811⁄2) | (851 ${ }^{\text {a }}$ ) | (89) | (93) | (9716) | (1011⁄2) | (106) |
| 6×5 | 148.1 | 154.8 | 161.7 | 168.9 | 176.5 | 184.4 | 192.6 | 201.2 | 210.3 |
| 6x6 | 150.3 | 157.0 | 164.1 | 171.4 | 179.1 | 187.1 | 195.5 | 204.2 | 213.3 |
| 6x7 | 152.5 | 159.3 | 166.5 | 173.9 | 181.7 | 189.8 | 198.3 | 207.2 | 216.5 |
| 618 | 154.8 | 161.7 | 168.9 | 176.5 | 184.4 | 192.6 | 201.2 | 210.3 | 219.7 |
| $6 \times 9$ | 157.0 | 164.1 | 171.4 | 179.1 | 187.1 | 195.5 | 204.2 | 213.3 | 222.9 |
| 7×0 | 159.3 | 166.5 | 173.9 | 181.7 | 189.8 | 198.3 | 207.2 | 216.5 | 226.2 |
| 7×1 | 161.7 | 168.9 | 176.5 | 184.4 | 192.6 | 201.2 | 210.3 | 219.7 | 229.5 |
| $7 \times 2$ | 164.1 | 171.4 | 179.1 | 187.1 | 195.5 | 204.2 | 213.3 | 222.9 | 232.9 |
| 7× 3 | 166.5 | 173.9 | 181.7 | 189.8 | 198.3 | 207.2 | 216.5 | 226.2 | 236.3 |
| 714 | 168.9 | 176.5 | 184.4 | 192.6 | 201.2 | 210.3 | 219.7 | 229.5 | 239.8 |
| $7 \times 5$ | 171.4 | 179.1 | 187.1 | 195.5 | 204.2 | 213.3 | 222.9 | 232.9 | 243.3 |
| 7×6 | 173.9 | 181.7 | 189.8 | 198.3 | 207.2 | 216.5 | 226.2 | 236.3 | 246.9 |
| 7×7 | 176.5 | 184.4 | 192.6 | 201.2 | 210.3 | 219.7 | 229.5 | 239.8 | 250.5 |
| 7×8 | 179.1 | 187.1 | 195.5 | 204.2 | 213.3 | 222.9 | 232.9 | 243.3 | 254.2 |
| 7x9 | 181.7 | 189.8 | 198.3 | 207.2 | 216.5 | 226.2 | 236.3 | 246.9 | 257.9 |
| $8 \mathbf{8}$ | 184.4 | 192.6 | 201.2 | 210.3 | 219.7 | 229.5 | 239.8 | 250.5 | 261.7 |
| $8 \mathbf{1}$ | 187.1 | 195.5 | 204.2 | 213.3 | 222.9 | 232.9 | 243.3 | 254.2 | 265.6 |
| $8 \times 2$ | 189.8 | 198.3 | 207.2 | 216.5 | 226.2 | 236.3 | 246.9 | 257.9 | 269.5 |
| $8 \mathbf{3}$ | 192.6 | 201.2 | 210.3 | 219.7 | 229.5 | 239.8 | 250.5 | 261.7 | 273.4 |
| $8 \mathbf{4} 4$ | 195.5 | 204.2 | 213.3 | 222.9 | 232.9 | 243.3 | 254.2 | 265.6 | 277.5 |
| $8 \mathbf{5}$ | 198.3 | 207.2 | 216.5 | 226.2 | 236.3 | 246.9 | 257.9 | 269.5 | 281.5 |
| $8 \times 6$ | 201.2 | 210.3 | 219.7 | 229.5 | 239.8 | 250.5 | 261.7 | 273.4 | 285.7 |
| $8 \mathbf{7}$ | 204.2 | 213.3 | 222.9 | 232.9 | 243.3 | 254.2 | 265.6 | 277.5 | 289.9 |
| $8 \mathbf{8}$ | 207.2 | 216.5 | 226.2 | 236.3 | 246.9 | 257.9 | 269.5 | 281.5 | 294.1 |
| $8 \mathbf{8 9}$ | 210.3 | 219.7 | 229.5 | 239.8 | 250.5 | 261.7 | 273.4 | 285.7 | 298.5 |
| $9 \mathbf{0}$ | 213.3 | 222.9 | 232.9 | 243.3 | 254.2 | 265.6 | 277.5 | 289.9 | 302.8 |
| $9 \mathbf{1}$ | 216.5 | 226.2 | 236.3 | 246.9 | 257.9 | 269.5 | 281.5 | 294.1 | 307.3 |
| $9 \times 2$ | 219.7 | 229.5 | 239.8 | 250.5 | 261.7 | 273.4 | 285.7 | 298.5 | 311.8 |
| $9 \mathbf{3}$ | 222.9 | 232.9 | 243.3 | 254.2 | 265.6 | 277.5 | 289.9 | 302.8 | 316.4 |
| $9 \mathbf{4}$ | 226.2 | 236.3 | 246.9 | 257.9 | 269.5 | 281.5 | 294.1 | 307.3 | 321.1 |
| $9 \mathbf{5}$ | 229.5 | 239.8 | 250.5 | 261.7 | 273.4 | 285.7 | 298.5 | 311.8 | 325.8 |

## All values are in mm (MondoPoint)

All Foot measurements are taken Barefoot, Men: Thin Dress Socks, or Women: Hose. If thicker socks are intended to be worn with a particular type of shoe or boot then the Lasts from which they are made from should have a slight increase in size made to them to compensate. A given percentage increase should be established for the type of sock to be worn for each shoe or boot design. Different increases in the Length, Width \& Girth will be needed, most for the Girth and least for the Length. These percentage increases should be applied to table values before being used for Lasts dimensions. 90.00 for the D Girth is for Non-Weight Bearing, the table values, while (93) is for Weight Bearing, a $3^{1 / 1 / 3} \%$ increase. The $31 / 3 \%(31 \div 30)$ increase has also been applied to the other Girth scalars.

Copy Ruler Image to - $-12773004.80 \mathrm{PD} \mid$
Clip Board and Paste into Image Editor.
Set Print D.P.I. to 304.8 and Print on $8^{1 / 2} 2^{\prime \prime} \times 14^{\prime \prime}$ Legal Size Paper or Card Stock. Cut Along Dotted Line at Top and Place on a Board with a Right Angle Back Stop.


## eXp7 Length to Width Graph



In the graph above are the plots of the Length \& Width increments. The Length \& Width are represented by the X \& Y axes. The sizes are represented by the vertical lines and the widths are are represented by the slanted horizontal lines. The smallest size, $\mathbf{6 \times 5}$, is on the Left side and the largest size, $9 \mathbf{x 5}$, is on the Right side. The narrowest width is on the bottom and the widest width is on the top. This illustrates the consistency of the Width:Length ratios for all sizes and width. To make the graph more illustrative the Width spacing has been normalized to the $\mathbf{V I}(\mathbf{C})$ width and all other widths plotted are the difference in reference to the VI Width. The squares (slightly rhombus-ed parallelograms) created maintain their aspect ratio through the size range. All the squares have the same aspect ratio for a given width spacing from the smallest to the largest sizes. For example the square bordered by the Width spacing of II \& IIII and the size spacing of $6 \mathbf{7} 5$ \& $6 \times 6$ has the same shape as the one bordered by sizes $9 \mathbf{I} 4$ \& $9 \mathbf{5}$, only enlarged. Likewise for Width spacing of IX \& $\mathbf{X}$ for sizes $\mathbf{6 \times 5}$ \& $\mathbf{6 x} 6$ and $9 \mathbf{Z} 49 \mathbf{5}$ the same is also true. Also notice the width lines are straight given that the $X \& Y$ values are non-linear incremented but the ratio between the values are fixed producing the straight lines.

To the right is the U.S. Brannock Width Variance Graph. Using a linear length and width increment causes these width deviations across the size range. Because of the width spreading for the smallest sizes there is probably no need to have the narrower or wider width specifications while the width squeezing for the largest sizes may not provide the needed range.


## eXp5 ${ }^{\text {TM }}$ MondoPoint 5 mm Replacement

Mainly intended for work shoes/boots and athletic footware, applying the same increment method used for eXp7 by incrementing the size by 5 mm @ 255 mm will produce 5 steps per inch between $9.7^{\prime \prime} \& 10.7^{\prime \prime}, \sim 10.2^{\prime \prime}$ avg.


Foot Increment Factor $=\sqrt{26 \div 25}=1.0198039$ $62 / 3 \%$ Toe Room $=1 / 0.9375=1.0 \overline{6}$

[^0]Widths

|  | AAA | AA | A | B | C | D | E | EE | EEE |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $\%$ | 27.94 | 29.64 | 31.43 | 33.34 | 35.36 | 37.50 | 39.77 | 42.18 | 44.74 |
| $7 \star 0$ | 58.6 | 62.1 | 65.9 | 69.9 | 74.1 | 78.6 | 83.4 | 88.4 | 93.8 |
| $7 \star 1$ | 59.7 | 63.4 | 67.2 | 71.3 | 75.6 | 80.2 | 85.0 | 90.2 | 95.6 |
| $7 \star 2$ | 60.9 | 64.6 | 68.5 | 72.7 | 77.1 | 81.7 | 86.7 | 92.0 | 97.5 |
| $7 \star 3$ | 62.1 | 65.9 | 69.9 | 74.1 | 78.6 | 83.4 | 88.4 | 93.8 | 99.5 |
| $7 \star 4$ | 63.4 | 67.2 | 71.3 | 75.6 | 80.2 | 85.0 | 90.2 | 95.6 | 101.4 |
| $7 \star 5$ | 64.6 | 68.5 | 72.7 | 77.1 | 81.7 | 86.7 | 92.0 | 97.5 | 103.4 |
| $7 \star 6$ | 65.9 | 69.9 | 74.1 | 78.6 | 83.4 | 88.4 | 93.8 | 99.5 | 105.5 |
| $7 \star 7$ | 67.2 | 71.3 | 75.6 | 80.2 | 85.0 | 90.2 | 95.6 | 101.4 | 107.6 |
| $7 \star 8$ | 68.5 | 72.7 | 77.1 | 81.7 | 86.7 | 92.0 | 97.5 | 103.4 | 109.7 |
| $7 \star 9$ | 69.9 | 74.1 | 78.6 | 83.4 | 88.4 | 93.8 | 99.5 | 105.5 | 111.9 |
| $8 \star 0$ | 71.3 | 75.6 | 80.2 | 85.0 | 90.2 | 95.6 | 101.4 | 107.6 | 114.1 |
| $8 \star 1$ | 72.7 | 77.2 | 81.7 | 86.7 | 92.0 | 97.5 | 103.4 | 109.7 | 116.3 |
| $8 \star 2$ | 74.1 | 78.6 | 83.4 | 88.4 | 93.8 | 99.5 | 105.5 | 111.9 | 118.7 |
| $8 \star 3$ | 75.6 | 80.2 | 85.0 | 90.2 | 95.6 | 101.4 | 107.6 | 114.1 | 121.0 |
| $8 \star 4$ | 77.1 | 81.7 | 86.7 | 92.0 | 97.5 | 103.4 | 109.7 | 116.3 | 123.4 |
| $8 \star 5$ | 78.6 | 83.4 | 88.4 | 93.8 | 99.5 | 105.5 | 111.9 | 118.7 | 125.8 |
| $8 \star 6$ | 80.2 | 85.0 | 90.2 | 95.6 | 101.4 | 107.6 | 114.1 | 121.0 | 128.3 |
| $8 \star 7$ | 81.7 | 86.7 | 92.0 | 97.5 | 103.4 | 109.7 | 116.3 | 123.4 | 130.9 |
| $8 \star 8$ | 83.4 | 88.4 | 93.8 | 99.5 | 105.5 | 111.9 | 118.7 | 125.8 | 133.5 |
| $8 \star 9$ | 85.0 | 90.2 | 95.6 | 101.4 | 107.6 | 114.1 | 121.0 | 128.3 | 136.1 |
| $9 \star 0$ | 86.7 | 92.0 | 97.5 | 103.4 | 109.7 | 116.3 | 123.4 | 130.9 | 138.8 |

Width Increment Factor $=(\text { Foot Increment Factor })^{3}=1.0605960588273$

# Girths 

|  | AAA | AA | A | B | C | D | E | EE | EEE |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Non-WB\% | 67.06 | 71.13 | 75.44 | 80.01 | 84.86 | 90.00 | 95.45 | 101.24 | 107.37 |
| WB\% | 69.30 | 73.50 | 77.95 | 82.68 | 87.69 | 93.00 | 98.64 | 104.61 | 110.95 |
|  |  |  |  |  |  |  |  |  |  |
| $7 \star 0$ | 140.6 | 149.1 | 158.1 | 167.7 | 177.9 | 188.6 | 200.1 | 212.2 | 225.0 |
| $7 \star 1$ | 143.3 | 152.0 | 161.2 | 171.0 | 181.4 | 192.4 | 204.0 | 216.4 | 229.5 |
| $7 \star 2$ | 146.2 | 155.0 | 164.4 | 174.4 | 185.0 | 196.2 | 208.1 | 220.7 | 234.0 |
| $7 \star 3$ | 149.1 | 158.1 | 167.7 | 177.9 | 188.6 | 200.1 | 212.2 | 225.0 | 238.7 |
| $7 \star 4$ | 152.0 | 161.2 | 171.0 | 181.4 | 192.4 | 204.0 | 216.4 | 229.5 | 243.4 |
| $7 \star 5$ | 155.0 | 164.4 | 174.4 | 185.0 | 196.2 | 208.1 | 220.7 | 234.0 | 248.2 |
| $7 \star 6$ | 158.1 | 167.7 | 177.9 | 188.6 | 200.1 | 212.2 | 225.0 | 238.7 | 253.1 |
| $7 \star 7$ | 161.2 | 171.0 | 181.4 | 192.4 | 204.0 | 216.4 | 229.5 | 243.4 | 258.2 |
| $7 \star 8$ | 164.4 | 174.4 | 185.0 | 196.2 | 208.1 | 220.7 | 234.0 | 248.2 | 263.3 |
| $7 \star 9$ | 167.7 | 177.9 | 188.6 | 200.1 | 212.2 | 225.0 | 238.7 | 253.1 | 268.5 |
| $8 \star 0$ | 171.0 | 181.4 | 192.4 | 204.0 | 216.4 | 229.5 | 243.4 | 258.2 | 273.8 |
| $8 \star 1$ | 174.4 | 185.0 | 196.2 | 208.1 | 220.7 | 234.0 | 248.2 | 263.3 | 279.2 |
| $8 \star 2$ | 177.9 | 188.6 | 200.1 | 212.2 | 225.0 | 238.7 | 253.1 | 268.5 | 284.8 |
| $8 \star 3$ | 181.4 | 192.4 | 204.0 | 216.4 | 229.5 | 243.4 | 258.2 | 273.8 | 290.4 |
| $8 \star 4$ | 185.0 | 196.2 | 208.1 | 220.7 | 234.0 | 248.2 | 263.3 | 279.2 | 296.1 |
| $8 \star 5$ | 188.6 | 200.1 | 212.2 | 225.0 | 238.7 | 253.1 | 268.5 | 284.8 | 302.0 |
| $8 \star 6$ | 192.4 | 204.0 | 216.4 | 229.5 | 243.4 | 258.2 | 273.8 | 290.4 | 308.0 |
| $8 \star 7$ | 196.2 | 208.1 | 220.7 | 234.0 | 248.2 | 263.3 | 279.2 | 296.1 | 314.1 |
| $8 \star 8$ | 200.1 | 212.2 | 225.0 | 238.7 | 253.1 | 268.5 | 284.8 | 302.0 | 320.3 |
| $8 \star 9$ | 204.0 | 216.4 | 229.5 | 243.4 | 258.2 | 273.8 | 290.4 | 308.0 | 326.7 |
| $9 \star 0$ | 208.1 | 220.7 | 234.0 | 248.2 | 263.3 | 279.2 | 296.1 | 314.1 | 333.1 |

Girth $=22 / 5 \times$ Width , Non-Weight Bearing (Non-WB\%)
Weight Bearing (WB\%) Compensation $=+31 ⁄ 3 \%$ (1.0 $0 \overline{3})$


[^0]:    A 6 step per inch increment (eXp6 ${ }^{\text {TM }} \otimes, \sqrt[6]{10^{1 / 2} \div 9^{1 / 2}} \approx 1.0168$ ) can also be realized providing a $1 / 2$ size Barleycorn increment @ $9^{2 / 5 \prime \prime}, \sim 5$ UK. Size $8 \boxtimes 0$ is the origin for a $10 "$ Foot. One in between eXp5 \& eXp7 that would be a good replacement for the Barleycorn system. eXp7 is best suited to replace the Paris Point system.

